Amendments to the Specification

Please amend the specification, as follows:

NB 4/25/07 [0027] ~~[0034]~~ The reactor was filled with 2 liters of ~~hexane~~ hexene and the temperature was increased to 80°C with agitation. 10 mg of a typical Zeigler-Natta catalyst was suspended in mineral oil and precontacted with 2 ml TEA1 solution (0.25 mmole/1 in ~~hexane~~hexene) in a dry box. Hydrogen and ethylene were admitted to the reactor at the flow rates of 2 standard liters per minute (SLPM) and 8 SLPM, respectively, and the reactor backpressure was maintained at 125 psi. The ZN catalyst-cocatalyst mixture was charged into the reactor. The reactor temperature and pressure were maintained for one hour. After one hour of polymerization, 3 mg of a metallocene catalyst, specifically titanocene dichloride, were charged into the reactor and polymerization was continued for another hour under the same reactor temperature and pressure. After transferring the polymer fluff slurry from the reactor to a flask, the solvent was removed and the polymer was collected as dry fluff.

FIG. 4 is a schematic diagram of a second alternative embodiment of an averaging circuit for the system of FIG. 2 in accordance with the present invention.

FIG. 5 is a simplified schematic showing how the system of FIG. 2 can be configured for operation in a measurement mode in accordance with the present invention.

FIG. 6 is a simplified schematic showing how the system of FIG. 2 can be configured for operation in a controller mode in accordance with the present invention.

FIG. 7 is a simplified schematic showing how the system of FIG. 2 can be configured for operation in a measurement mode for measuring true power in a nonlinear load in accordance with the present invention.

FIG. 8 is a schematic diagram of a preferred embodiment of a wideband amplifier cell in accordance with the present invention suitable for use in a practical implementation of the circuit of FIG. 2.

FIG. 9 shows the large-signal gain function of the wideband amplifier cell of FIG. 8.

FIG. 10 is a schematic diagram of an embodiment of a four-quadrant multiplier in accordance with the present invention for use in a practical implementation of the circuit of FIG. 2.

FIG. 11 is a simplified schematic diagram of an embodiment of an averaging circuit in accordance with the present invention for a practical implementation of the circuit of FIG. 2.

FIG. 12 is a schematic diagram showing more details of a practical embodiment of the averaging circuit of FIG. 11.

FIG. ~~14~~ 13 shows a preferred arrangement of differential attenuators and multipliers in accordance with the present invention for a practical implementation of the circuit of FIG. 2.

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FIG. 14 is a simplified schematic diagram of an embodiment of a current source in accordance with the present invention suitable for use in the averaging circuit of FIGS. 11 and 12.

FIG. 15 is a schematic diagram showing more details of a practical embodiment of the current source of FIG. 14 in accordance with the present invention.

FIG. 16 is a schematic diagram of a conventional current mirror.

FIG. 17 illustrates the output characteristics of the current mirror of FIG. 16.

FIG. 18 is a schematic diagram showing a preferred embodiment of an averaging circuit for a practical implementation of an RMS-DC converter in accordance with the present invention.